













Bezier Curves: de Casteljau construction	n
• L+1 control points: $\mathbf{P}_0, \mathbf{P}_1, \mathbf{P}_2, \mathbf{P}_3, \dots \mathbf{P}_L$	
• L iterations of replacing points by affine combinations	
 (initial points are the control points) 	
– new point is affine combination of previous pair of	points
 Number of points decreases by 1 	
Repeat for every t value	
$P_{i}^{4}(t) = (1 - t) P_{i}^{3}(t) + t P_{i+1}^{3}(t)$	
 $\mathbf{P}_{i}^{L}(t) = (1 - t) \mathbf{P}_{i}^{L-1}(t) + t \mathbf{P}_{i+1}^{L-1}(t)$	
Upper Index K: Iteration Number. K = 1,L Lower index i: point number: i = 0, L-K	















Wish List for Blending Functions

• be easy to compute and numerically stable

– Polynomials, with small degrees

- sum to one at every *t* in [a,b]: $\Sigma R_k(t) = 1$
- have small support to offer local control
- interpolate certain control points, chosen by designer
- be smooth enough: Have continuous derivative
 - Derivatives = 0 at t=0, 1 (no jumps of R_k there)
 - Try cubic polynomial: $R(t) = at^3 + bt^2 + ct + d$
 - No solution for R(0) = R'(0) = R(1) = R'(1)





Spline Functions

• An *n*th-degree spline function is a piecewise polynomial of degree *n*

- With the (n-1) derivative is continuous at knots

- The example g(t) is a quadratic spline
 - It is a piecewise polynomial of degree 2 and has a continuous first derivative everywhere
- From a spline function g(t) we build the blending functions, $g_k(t)$







Properties of the Curve

- The designer has some local control of the curve shape
- since the support of the blending functions is length 3
- the curve pass through midpoints of the polygon edges
 - The curve has intuitive geometric properties.
- each blending function is 1-smooth,
 - whole curve is 1-smooth (1'st derivative is continuous)
- No points on the curve are interpolated
- All polynomials are of degree two,
 - so they are fast and stable to compute.
- The degree of the polynomials does not depend on the number of control points.
 - The technique works for any number of control points

More General Blending Functions

- We need more control of the curve shape
 - it must bend more and be smoother than just 1-smooth.
- This suggests moving to cubic polynomials
- We also want the designer to be able to specify which control points are interpolated.
- And we want a single algorithm that would encompass all of the design techniques described above including Bezier curves.
- So we want to develop more general families of blending functions that meet all the properties discussed in the earlier wish list.



More General Blending Functions (3) • Each blending function $R_k(t)$ is a piecewise polynomial - zero up to time t_k , then non-zero over several spans in the knot vector, and then returns to zero again. each $R_k(t)$ is a spline function • ensures a certain level of smoothness at all t in its support $R_2(t)$ $R_3(t)$ $R_1(t)$ $R_0(t)$ to t₁ t₂ t3 t4 t5 t₆ t7 knot vector

B-spline (Basis) Functions

• B-spline functions of order n: $b_{i,n}$ i = 0, 1, ...

- pieces of polynomials of degree n-1

- Two most important cases
- n = 3, underlying polynomials of degree 2

- quadratic B-splines.

- n = 4, underlying polynomials of degree 3
 - cubic B spline
- B-splines of any order can be constructed

B-spline Basis Functions (2)• Define a knot vector:• $\mathbf{T} = (t_0, t_1, t_2 \dots t_m)$ • $\mathbf{T} = (t_0, t_1, t_2 \dots t_m)$ • A curve is defined by:• A curve is defined by:• a set of (m-n) B-spline functions of order n $- b_{i,n}(t), i = 0, 1, \dots m-n-1$ - and (m-n) control points $\mathbf{P}_i, i = 0, 1, \dots m-n-1$ • $\mathbf{P}(t) = \Sigma \mathbf{P}_i b_{i,n}(t)$ $t_n \le t \le t_{m-n}$ • sum over $i = 0, 1, \dots m-n-1$



B-splines: Usage and construction

$$S(t) = \sum_{i=0}^{m-n-1} \mathbf{P}_i b_{i,n}(t) , t \in [t_n, t_{m-n}]$$

$$b_{j,0}(t) := \begin{cases} 1 & \text{if } t_j \leq t < t_{j+1} \\ 0 & \text{otherwise} \end{cases}$$

$$b_{j,n}(t) := \frac{t-t_j}{t_{j+n}-t_j} b_{j,n-1}(t) + \frac{t_{j+n+1}-t}{t_{j+n+1}-t_{j+1}} b_{j+1,n-1}(t).$$



• quadratic B-spline curve • Each triplet of control points define a segment $S_{i}(t) = \begin{bmatrix} t^{2} & t & 1 \end{bmatrix} \frac{1}{2} \begin{bmatrix} 1 & -2 & 1 \\ -2 & 2 & 0 \\ 1 & 1 & 0 \end{bmatrix} \begin{bmatrix} p_{i-1} \\ p_{i} \\ p_{i+1} \end{bmatrix}$ • Cubic B-spline curve • Each quartet of control points define a segment $S_{i}(t) = \begin{bmatrix} t^{3} & t^{2} & t & 1 \end{bmatrix} \frac{1}{6} \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 0 & 3 & 0 \\ 1 & 4 & 1 & 0 \end{bmatrix} \begin{bmatrix} p_{i-1} \\ p_{i} \\ p_{i+1} \\ p_{i+2} \end{bmatrix}$



Standard Knot Vector

- The **standard knot vector** for a B-spline of order *n* begins and ends with a knot of multiplicity *n* and uses unit spacing for the remaining knots.
- Example
- 8 control points
- and we want to use cubic (n = 4) B-splines.
- The standard knot vector turns out to be
- $\mathbf{T} = (0, 0, 0, 0, 1, 2, 3, 4, 5, 5, 5, 5)$
 - i.e 6 different knots
- those at the ends are multiple knots





Standard Knot Vector (4)

- Standard knot vector for (*L*+1) control points and order-*n* B-splines
- L+n+1 knots, denoted as t_0, \ldots, t_{L+n} .
- The first *n* knots, t_0, \ldots, t_{n-1} , all share the value 0.
 - The first *n* blending functions start at t = 0
- Knots t_n,..., t_L increase in increments of 1, from value 1 through value L - n+1.
- The final *n* knots, t_{L+1}, \ldots, t_{L+n} , all equal L n + 2.



Non Uniform Rational B-splines (NURBS)

$$P(t) = \sum_{k=0}^{L} P_k R_k(t)$$

- blending functions R_k are weighted B-splines
- Weights: $\{w_0, w_1, ..., w_L\}$

$$P(t) = \frac{\sum_{k=0}^{L} w_k P_k N_{k,m}(t)}{\sum_{k=0}^{L} w_k N_{k,m}(t)}$$

- $N_{k,m}$ are m'th order, non-uniform knots, B-splines
- If all W are the same, we get the usual B-splines



- NURBS are invariant under **perspective transformation M**
- M = (m1|m2|m3|m4)
- drawing a perspective projection of a NURB curve
- find the perspective projection of each of its control points
- then draw the curve using the *same* blending functions
 - The weights must be adjusted as well







Piecewise Cubic Polynomials (4)

Example

- 3 control points: (1,1), (4, 3), (0,3)
- a curve consisting of two cubic segments, $\mathbf{R}_0(t)$ and $\mathbf{R}_1(t)$
- Segments join at (4,3)
- $R_0(t)$ passes through (1,1) at t = 0 and through (4,3) at t = 1.

- its slope is (1,0) at t = 0 and is (0, S) at t = 1

• $R_1(t)$ passes through (4, 3) at t = 0 and through (0,3) at t = 1.

- Its slope is (0, S) at t = 0 and (0, 1) at t = 1

• S varies to see the effect of slope changes in the curve

	Example (2)
•	Segment 0:
•	$x_0(t) = -5t^3 + 7t^2 + T + 1$
•	$y_0(t) = (S - 4)t^3 + (6 - S)t^2 + 1$
•	Segment 1:
•	$x_1(t) = 8t^3 - 12t^2 + 4$
•	$y_1(t) = (S+1)t^3 - (2S+1)t^2 + St + 3$
•	Now change S, look near joint (4,3)
•	Only y behavior changes
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Natural Cubic Splines • Setting derivative values U_k , V_k • Demand $x_k''(t)$, $y_k''(t)$ to be continuous at joints • Second derivative of segment: $x_k''(t) = 6a_kt + 2b_k$ • Require: $x_{k-1}''(1) = x_k''(0) = 0$ $-6a_{k-1} + 2b_{k-1} = 2b_k$ k in [0, L-1] $-U_{k-1} + 4 U_k + U_{k+1} = 3(X_{k+1} - X_{k-1}), k in <math>[1, L-1]$ • at endpoints: Impose $x_k''(0) = x_{L-1}''(0) = 0$ • $b_0 = 0; \quad 3a_{L-1} + b_{L-1} = 0$ • $2U_0 + U_1 = 3(X_1 - X_0); \quad 2U_L + U_{L-1} = 3(X_L - X_{L-1})$



Simple Catmull-Rom Splines

- another method to fix the slopes at the joints.
- 1. require curve to be 1-smooth at the joints (as before)
- 2. do not require that the curve will be 2-smooth there.

- Hoping to get local control of the curve's shape.

- slopes at joints determined by positions of their neighbors
- Simplest approach: force slope vector at P_k , $\underline{P'}(t_k)$, to be proportional to the vector from P_{k-1} to P_{k+1} :

 $- \underline{\mathbf{P'}}(\mathbf{t}_k) = \mathbf{m}(\mathbf{P}_{k+1} - \mathbf{P}_{k-1}) \qquad \text{usually } \mathbf{m} = \frac{1}{2}$

• curve at P_k moves parallel to the direction $P_{k-1}P_{k+1}$



Catmull-Rom tension parameter

- Aim: greater control of the shape at each joint
- By parametrising *m*: $\underline{\mathbf{P}}'(\mathbf{t}_k) = \frac{1}{2}(1 \mathbf{v}_k)(\mathbf{P}_{k+1} \mathbf{P}_{k-1})$
- adjusting magnitude of the slope **P**'(*t*) not its direction.
- Normally $-1 \le v_k \le 1$, but it can have any value
- (a) $v_2 = 1$, slope = 0 at the joint, curve straightens at joint
- (b) $v_2 = -1$; the curve is more "slack" at the joint









Modeling Curved Surfaces

- Various surfaces can be design by using B-splines
- B-spline ruled surfaces
- B-spline surfaces of revolution
- Bezier surface patches
- B-spline patches
- NURBS surfaces
- Basic idea: Surfaces defined and managed by a set of control points



Bezier Ruled Surfaces

- $P(u, v) = (1 v) P_0(u) + v P_1(u)$.
- Recall Bezier curve

$$P(t) = \sum_{k=0}^{L} P_{k} B_{k}^{L}(t)$$

• Apply this to $P_0(u)$, $P_1(u)$, (with L = 3, cubic Bezier curves)

$$P(u,v) = \sum_{k=0}^{3} \left((1-v) P_{k}^{0} + v P_{k}^{1} \right) B_{k}^{3}(u)$$

• B-spline or NURBS curves could also be used

B-spline Surfaces of Revolution

- a profile C(v) = (X(v), Z(v)) is revolved about the *z*-axis.
- The resulting surface, P(u, v)

$$- \mathbf{P}(\mathbf{u}, \mathbf{v}) = (\mathbf{X}(\mathbf{v})\cos(\mathbf{u}), \mathbf{X}(\mathbf{v})\sin(\mathbf{u}), \mathbf{Z}(\mathbf{v}))$$

- Select L+1 control points (X_k, Z_k)
- create the profile curve

$$- (X(v), Z(v)) = \sum (X_k, Z_k) b_{k,n}(v) \quad \text{sum over } k = 0, ..L$$

• $\mathbf{P}(u,v) = \Sigma(X_k \cos(u), X_k \sin(u), Z_k) b_{k,n}(v)$ sum over k = 0..L



Bezier Surface Patches

Start with a Bezier curve, managed by control points
 P_k k = 0, 1, ...L

$$P(t) = \sum_{k=0}^{L} P_{k} B_{k}^{L}(t)$$

 Now move each P_k along another Bezier curve, managed by control points P_{i,k}

$$P(u,v) = \sum_{k=0}^{3} P_{k}(v)B_{k}^{3}(u) = \sum_{k=0}^{3} \left(\sum_{i=0}^{2} P_{i,k}B_{i}^{3}(v)\right)B_{k}^{3}(u)$$

fixed u ("u contours") are quadratic Bezier curves
Fixed v ("v contours") are cubic Bezier curves





B-spline, NURBS Patches • B-spline patches: greater control $P(u,v) = \sum_{i=0}^{M} \sum_{k=0}^{L} P_{i,k} N_{i,m}(u) N_{k,n}(v)$ • NURBS patches $P(u,v) = \frac{\sum_{i=0}^{M} \sum_{k=0}^{L} w_{i,k} P_{i,k} N_{i,m}(u) N_{k,n}(v)}{\sum_{i=0}^{M} \sum_{k=0}^{L} w_{i,k} N_{i,m}(u) N_{k,n}(v)}$



